

# Grey-box Modelling of a Quadrotor Using Closed-loop Data

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Saab Aeronautics

Aerospace Technology Congress 2016  
2016-10-12

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- 2 System Identification
- 3 Result
- 4 Conclusions

## Background

In control design, there is a need of a model describing the dynamics of the system.

Often, a physical model is complex and/or inaccurate due to simplifications.

## Goal

Find a simple mathematical model describing the dynamics of a hovering quadrotor.

## Approach

Use measured input and output data to estimate a model: System Identification

### Introduction

The Quadrotor

### System Identification

Grey-box Modelling

Closed-loop  
Identification

Two-stage method

### Result

### Conclusions

## System Overview

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Photo: M.Blomberg

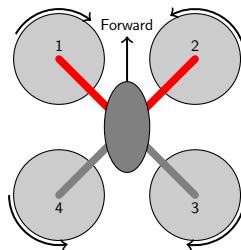
- Accelerometer
- Gyroscope
- Magnetometer
- Voltage to motors
- Joystick reference signals

# The Quadrotor

## Maneuverability

- Four control signals, one for each motor
- Maneuverability due to thrust differences
- Roll input:

$$u_\phi = \frac{1}{4} (u_1 + u_4 - u_2 - u_3)$$

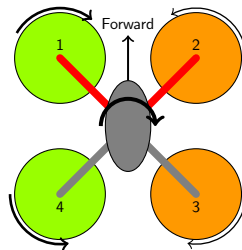


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# System Identification

## Main idea

An approach to create a mathematical model of a system

- Assume one or more mathematical structures (equations)
- The structures have a set of unknown values, called parameters ( $\Theta$ )
- Estimate  $\Theta$  using collected input-output data

# System Identification

## Grey-box Modelling

### Black-box Modelling

- Estimated from input-output data
- No connection to the underlying physics
- Model restricted by order

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- Structure from physical relations
- Physical meaning
- Model restricted by structure

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$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \end{pmatrix} = \begin{pmatrix} \Theta_1 & \Theta_2 \\ \Theta_3 & \Theta_4 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} + \begin{pmatrix} \Theta_5 \\ \Theta_6 \end{pmatrix} u$$
$$y = (\Theta_7 \quad \Theta_8) \begin{pmatrix} x_1 \\ x_2 \end{pmatrix}$$

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$$\begin{pmatrix} \dot{p} \\ \dot{T}_\phi \end{pmatrix} = \begin{pmatrix} \Theta_1 & \Theta_2 \\ \Theta_3 & \Theta_4 \end{pmatrix} \begin{pmatrix} p \\ T_\phi \end{pmatrix} + \begin{pmatrix} \Theta_5 \\ \Theta_6 \end{pmatrix} u_\phi$$
$$y = \begin{pmatrix} 1 & 0 \end{pmatrix} \begin{pmatrix} p \\ T_\phi \end{pmatrix}$$

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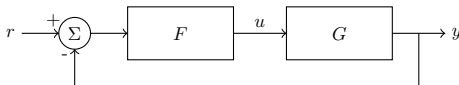
Parameters estimated using the Prediction-Error Method (PEM)

# System Identification

## Closed-loop Identification

## Closed-loop system

A system with output feedback.

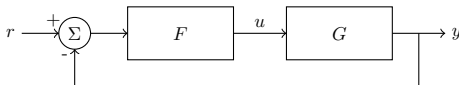


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## Closed-loop Identification

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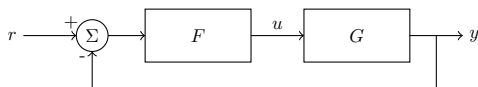


## Approaches to closed-loop identification

- Direct approach
  - First approach
  - Ignore the feedback
- Take the controller into consideration
  - For example: the *Two-stage method*

# System Identification

## Two-stage method



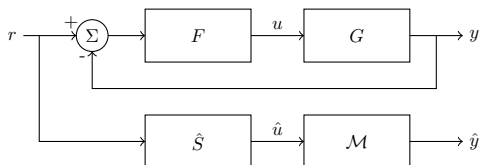
1. Estimate a model  $\hat{S}$  from  $r(t)$  to  $u(t)$

$$\hat{S} \approx \frac{F}{1 + FG}$$

- 2a. Simulate the input:  $\hat{u}(t) = \hat{S}r(t)$
- 2b. Use the **simulated** input and **measured** output to estimate the model  $\mathcal{M}$

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## Two-stage method



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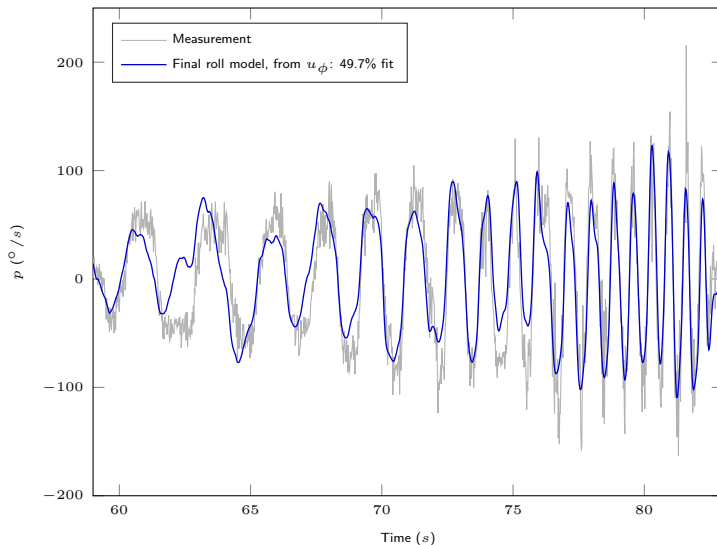
# Roll Rate Model

## Resulting Model

- Models estimated using both the direct approach and the two-stage method
- Similar results from both methods
- Direct approach model chosen due to simplicity

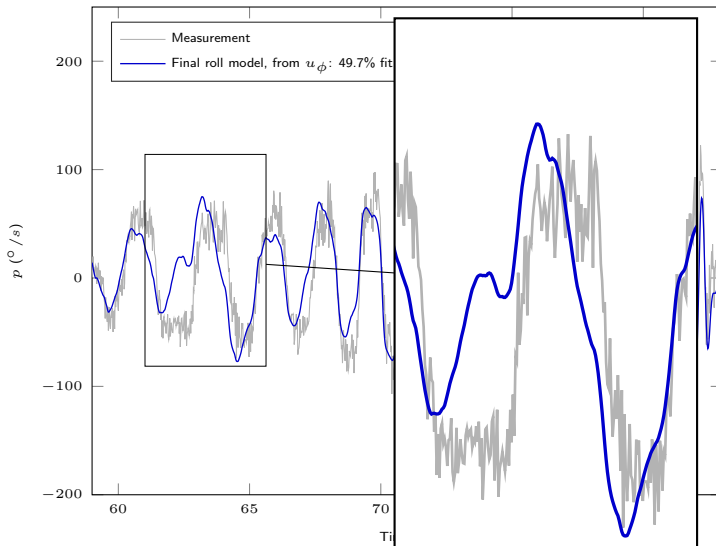
# Roll Rate Model

Simulation from  $u_\phi$



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Simulation from  $u_\phi$



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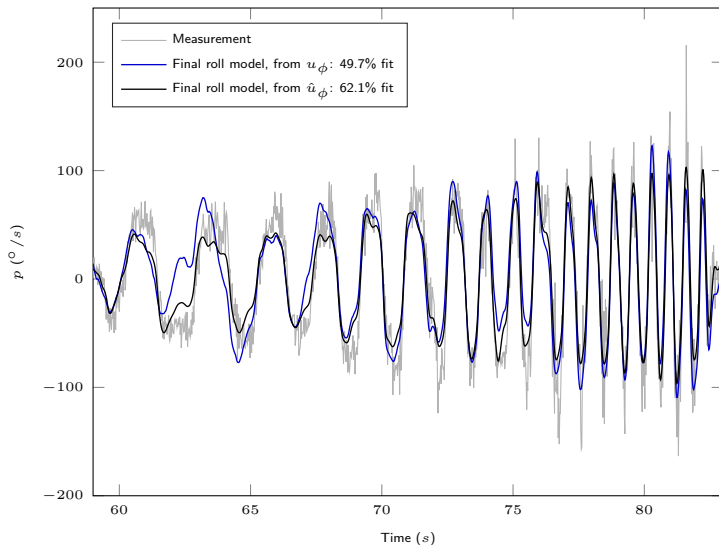
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Simulation from  $u_\phi$



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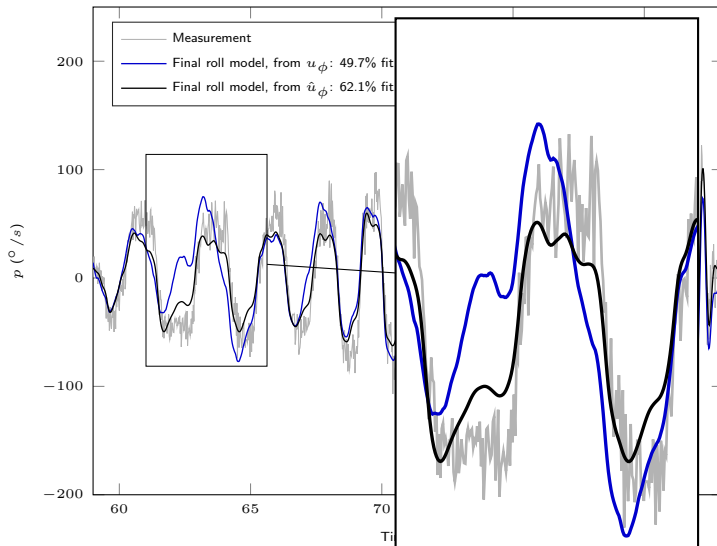
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Simulation from  $u_\phi$



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# Conclusions

- The direct approach is good enough.
- The two-stage method provides insights to the closed-loop system.
- For control design, this model is good enough.

# The End

Thank you!