



ELEMENTARY SOURCE ARRAYS IN THE SYNTHESIS OF ACOUSTIC FIELDS DUE TO TURBULENT FLUCTUATIONS AROUND FUSELAGE PANELS

Clinton André Merlo

Alexander Mattioli Pasqual

Eduardo Bauzer Medeiros (*)

Federal University of Minas Gerais (UFMG)

BRAZIL



AEROSPACE TECHNOLOGY CONGRESS 2016

Swedish aerospace technology in a globalised world

October 11-12, 2016 - Solna - Stockholm



Summary

UFMG

- **Introduction and Motivation**
- **The Cabin Acoustic Problem**
- **General method**
- **Monopole Source Synthesis Optimization**
- **Some Results**
- **Main Conclusions**



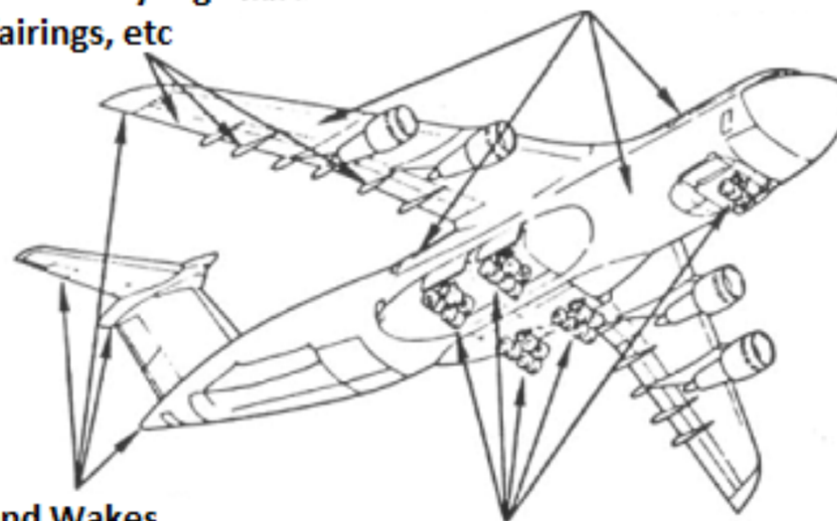
Motivation

Together with the more demanding quieter cabins:

- **New construction techniques and technology have modified the environment inside an aircraft**
- **Cost effective and more flexible evaluations are needed.**

Wing Unsteady Aerodynamic
Forces modified by High Lift
devices, fairings, etc

Boundary Layer Flow
over the Entire Airframe



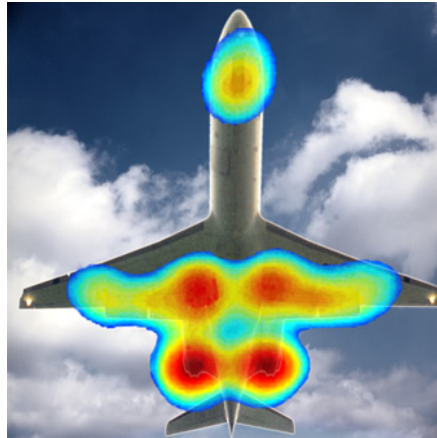
Vortices and Wakes
originating from
trailing edges

Flow around landing gear
Wheels, Doors and Wells

OUTSIDE NOISE SOURCES

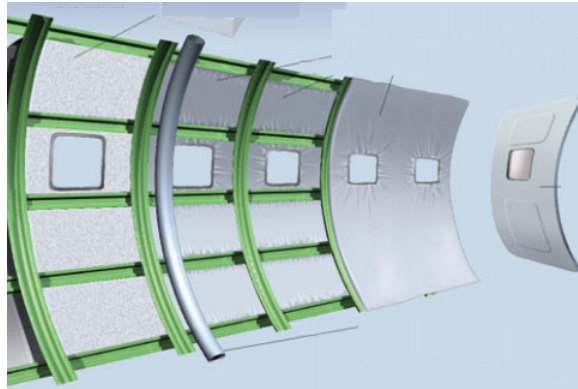
plus

INTERNAL NOISE SOURCES (ECS etc)



SOURCE

- **Engine Flow**
- Engine Vibration
- Engine Combustion
- **Body Boundary Layer**
- **High Lift Devices**
- **Undercarriage**
- E C S



X

PATH

=



RECEIVER

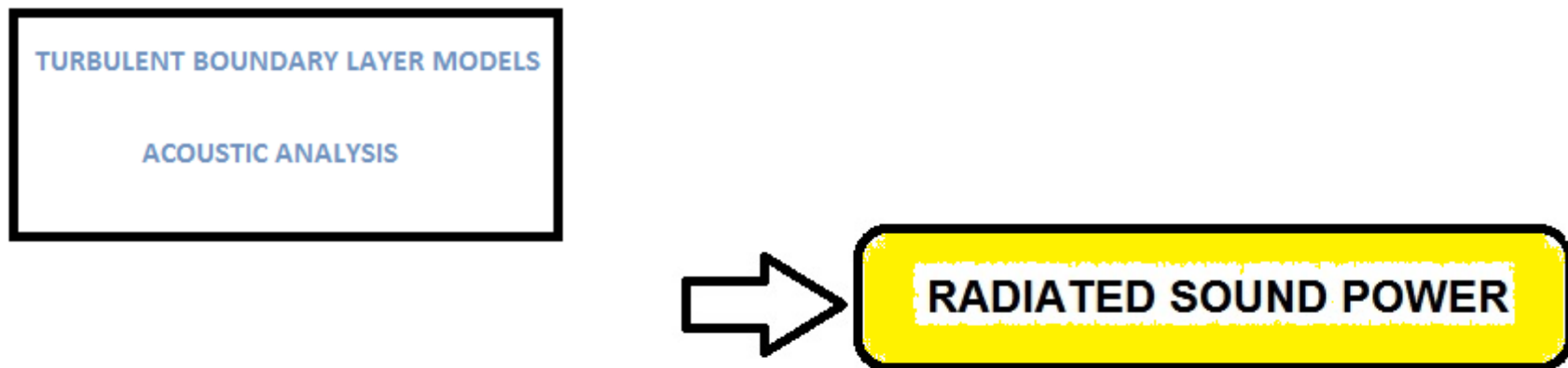
- Internal Noise
- Vibration
(stronger in piston engine)



Boundary Layer Noise

UFMG

- **Global Two Dimensional Turbulent Boundary Layer Models**
- **The problem to be looked at cruising regime!**





Obtaining TBL models

UFMG

- **OBJECTIVE: To obtain → Total Energy**
- **A VARIETY OF METHODS: going back to the 1960s**
- **INPUTS: Flight regimes (Re, Ma, etc)**
- **ALSO: Vortex Shedding (Sh,etc)**



Results: TBL models



- **STATISTICS:** Statistics → Mean Square Pressure+(Single) Wall Pressure Spectrum + Normalized Wave Number Spectrum. (the need to obtain total energy and spectrum distribution)
- **MODELING:** Analytic/Empiric + Numeric Methods (LES/DES models, etc)
- **QUALITY OF MODELS:** Strong dependence on flight conditions
- **RESULTS:** → Power Spectral Density (PSD) outputs



The Point: New Demands

UFMG

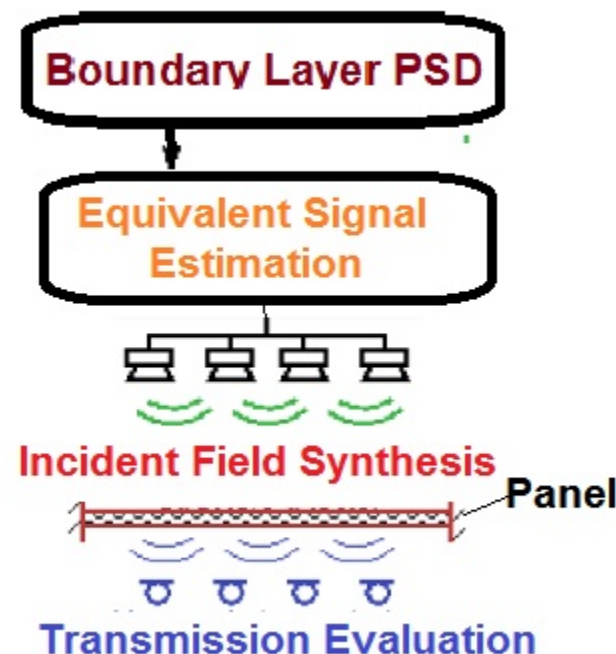
- **Increased use of composite materials, with different damping properties, and also:**
- **Substantial modification in panel stiffness**
- **Change in construction techniques have also modified “interference” damping!**
- **Transmission and Radiation changes require improved corrections**



Evaluation Strategy

UFMG

- Flight or Wind Tunnel Testing are expensive
- Source control can be a problem
- Therefore: The introduction of an equivalent source array!





Implementing simulated TBL UFMG

- ✓ **Aerodynamic improvements (particularly for high lift devices) is a key issue but that is another research^(*)**
- ✓ **Present models for Turbulent Boundary Layer (TBL) noise are quite reasonable**
- ✓ **Monopole source modeling^(*) is efficient and easier to achieve**





Monopole modeling

UFMG

Monopole Complex Free Field Sound Pressure

$$p(r, k) = -j \omega \rho_0 Q \frac{e^{jkr}}{4\pi r}$$

And the Superposition using the Image Method

$$p(r^-, k) + p(r^+, k) = -j \omega \rho_0 Q \left(\frac{e^{jkr^-}}{4\pi r^-} + \frac{e^{jkr^+}}{4\pi r^+} \right)$$

Resultant Pressure for an array having n monopoles

$$p(x_j, y_j, z_j, k) = -j \omega \rho_0 \sum_{i=1}^n Q_i \left[\frac{e^{jkr_i^-}}{4\pi r_{ij}^-} + \frac{e^{jkr_i^+}}{4\pi r_{ij}^+} \right]$$

General Propagation Model having m measurement points over a panel

$$\mathbf{A} \mathbf{q} = \mathbf{p} \text{ (Transfer Matrix } \mathbf{A})$$



Acoustic Synthesis

UFMG

Acoustic Synthesis (inverse Optimized Problem)

$$\min \|Aq - p\|_2$$

Truncated Singular Value Decomposition to achieve Matrix Conditioning

$$q_{TSVD} = \sum_{i=1}^k \sigma_i^{-1} (u_i^H p) v_i = (A_k^H A_k)^{-1} A_k^H p$$



Sound Power Model

Particle Velocity obtained from superposition
and Sound Power Model

$\mathbf{B}\mathbf{q} = \mathbf{u}$ (Velocity Transfer $m \times n$ Matrix \mathbf{B})

Sound Power Model over a surface S

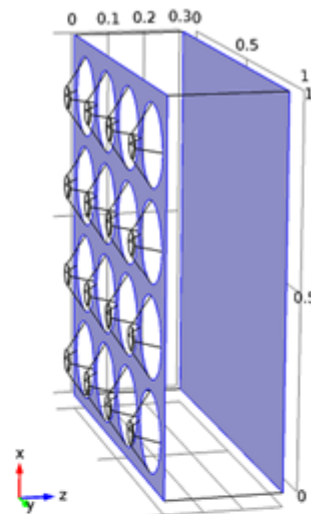
$$\Pi \approx \frac{\Delta s}{2} \mathbf{q}^H \mathbf{B}^H \mathbf{A} \mathbf{q}$$

$$\mathbf{W} = \mathbf{B}^H \mathbf{A}$$

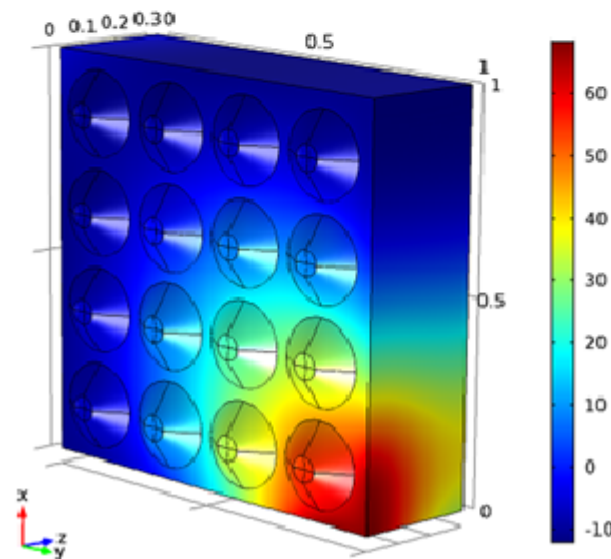
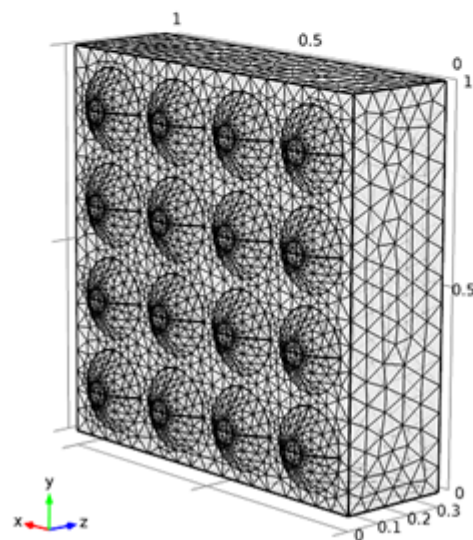


Equivalent Source Array

UFMG



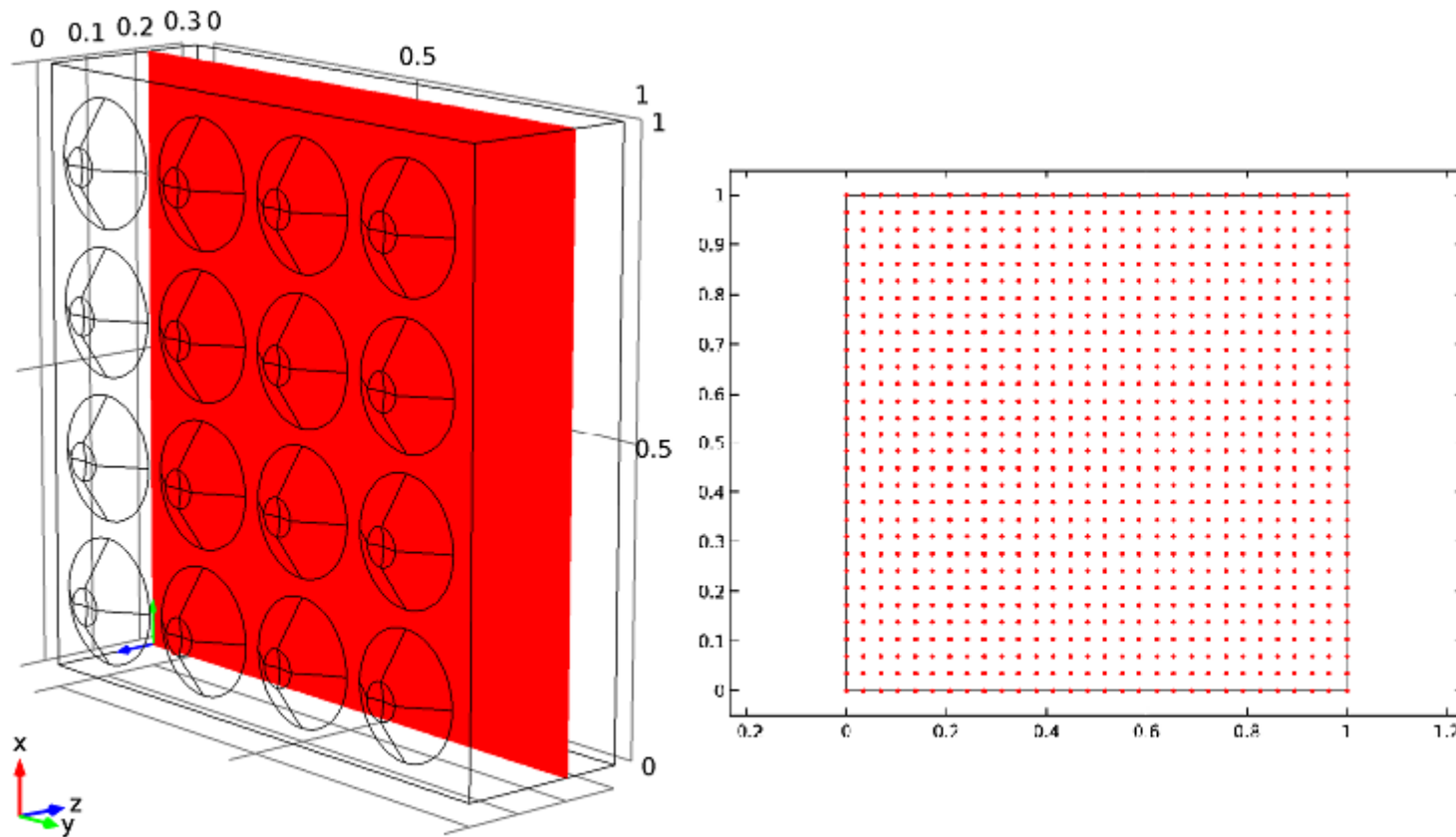
freq(1)=200 Hz Surface: Total acoustic pressure field (Pa)





Panel Excitation

UFMG





PROBLEMS?

UFMG

- **Acoustic Chamber requirements to provide free field conditions (*)**
- **Electric power and transducer requirements can be problem, requiring scaling (**)**



Main Conclusions



- **New construction Technologies require renewed assessment of aircraft cabin noise evaluation which can be made easier with:**
- **(Simulated) Monopole Acoustic Source Synthesis, minimizing Wind Tunnel and Flight Testing**
- **However for actual testing both electric power and transducer requirements have to be carefully considered**
- **The research continues.....**



Thank you very much



Aerospace Engineering Team
UFMG

ebauzerm@ufmg.br