

THE EFFECT OF MICROSTRUCTURE AND DEFECTS ON MECHANICAL PROPERTIES OF TI6AL4V WELDS PRODUCED BY DIFFERENT PROCESSES





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#### BACKGROUND



Fabricated aeroengine components enable

- 1. design of lighter aeroengines with improved performance
- 2. Lower buy-to-fly ratio

Lower environmental impact and economical benefits

High quality welds are prerequisite for fabrication technologies

#### WELDING OF TITANIUM ALLOYS - TI6AL4V

Most used titanium alloy in aerospace industry

Reactivity at elevated temperatures

Has the best weldability of  $\alpha + \beta$  alloys

Single phase solidification

 Highly resistant to solidification and liquation cracking related cracking

Complex microstructures in continuous cooling Porosity



#### WELDING PROCESSES



#### FATIGUE IN WELDS

Lower fatigue performance and high scatter due to

- Discontinuations
- Defects
- Brittle phases
- Distortions
- Residual stresses
- Stress concentrations



Incomplete penetration

### AIM OF THE WORK

What kind of microstructures are produced with different weld processes? What kind of defects exist for different processes(/parameters)? How do different microstructures effect on mechanical properties? What size and distribution of defects effect mechanical properties?

### EXPERIMENTAL PROCEDURE

#### **Material**

4 mm thick AMS4911 Ti-6Al-4V sheet

#### Welding

- TIG, PAW, LBW, EBW
- Post weld heat treatment at 704°C for 2h
- Machining

#### Mechanical testing

- Tensile testing
- Fatigue testing
  - Load controlled at at RT and 250°C in air
  - R=0

#### Microstructure

OM, SEM, microhardness

#### Fractography

Location and size of crack initiation sites



#### MACROSTRUCTURE



#### FUSION ZONE MICROSTRUCTURE



	TIG	PAW	EBW	LBW
FZ width	12.3/7.	7.3/5.8	3/3 mm	3/1.8 mm
top/bott om	5mm	mm		
HAZ width	2 mm	1.8 mm	1.8 mm	1.6 mm
Prior-β grain size	3 mm	2 mm	1.5 mm	1 mm
GB-α	1	1	Thin/	Thin/
	µm/conti	µm/conti	uncontinuo	uncontinu
	nuous	nuous	US	ous
α lath	1.2-1.3	1.2-1.3	0.8-1 µm	0.8-1 µm
spacing	μm	μm		

### MICROSTRUCTURE - EBSD

- Euler angle presentation
- PAW basket weave
- TIG combination of colony and basket weave structure





#### **MICROHARDNESS**



Distance from weld centre line (µm)

#### **TENSILE PROPERTIES**

Process	Test temp (°C)	Yield strength (normali zed)	UTS (normali zed)	Elongati on A4 (%)
Base material	20	0.95	1.00	16,4
Base material	250	0.72	0.78	17,8
EBW	20	0.92	0.99	10
EBW	250	0.67	0.78	15
LBW	20	0.91	0.97	10
LBW	250	0.66	0.76	12
TIG	20	0.85	0.94	7
TIG	250	0.58	0.73	14
PAW	20	0.84	0.93	9
PAW	250	0.58	0.71	14



### LOW CYCLE FATIGUE

How do different microstructures effect on mechanical properties? What size and distribution of defects effect mechanical/LCF properties?



## EFFECT OF WELD GEOMETRY





#### FRACTOGRAPHY TIG&PAW





#### FRACTOGRAPHY EB



#### FRACTOGRAPHY LBW



#### FRACTOGRAPHY SUMMARY

Size [µm]	TIG	PAW	EBW	LBW
Surface				
initiation	3	2	24	9
0-100	3	3	4	15
100-200	10	3	-	3
200-300	6	-	-	-
300-400	4	-	-	-
400-500	1	-	-	-
600-700	-	LOF	-	3



#### EFFECT OF PORE SIZE AND LOCATION



#### EFFECT OF TEMPERATURE







### X-RAY MICROSCOPY

Zeiss Xradia Versa 520

Optical magnification system (in contrast to x-ray tomography)

Scan times in examples 4-12 hrs

Voxel size down to 70 nm

#### CASE: TIG WELD FATIGUE SAMPLE



• Cycles to failure 13166

#### CASE: LASER WELD SAMPLE



Discontinued after 432 000 cycles No failure Largest pore 114 µm Smallest pore detected



# CONCLUSIONS

Pores initiated cracks on nearly all the samples in PAW and TIG welds whereas in LB and EB welds most samples had crack initiation at the surface

Large pores and pores close to surface were the most detrimental to fatigue life

Microstructure & hardness have an effect on fatigue performance

- EB&LBW had better fatigue performance than TIG&PAW
- LBW had lot of porosity but only large pores initiated crack

### FUTURE WORK

Predict fatigue life using LEFM XCT to identify critical defects

Effect of small boron addition in microstructure of Ti64 welds



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